Exercises

Port-Hamiltonian modelling and passivity-based control of physical systems. Theory and applications

Exercise #1

The figure shows the physical part of a load-positioning system without the sensors and the controller electronics that control the voltage source.



- 1. You are to make a bond graph model of the system, including the following effects:
 - A. The voltage is a controlled effort source. Indicate this by including a signal or active bond with a double arrow impinging on an effort source.
 - B. The dc motor has inductance and resistance in the armature coils.
 - C. Include a rotary inertia for the motor armature and the screw drive.
 - D. Use a resistor to model the friction moment associated with the motor and the screw drive.
 - E. A constant S relates the angular velocity of the screw with the nut: $V_1 = S \omega$.
 - F. The tube connecting the nut with the load mass is elastic with a spring constant k.
 - G. The load mass has significant friction with the ground.
- 2. Write down the final system in port-Hamiltonian form.
- 3. Suppose that the control input is the torque τ generated by the dc motor. Develop an energyshaping control law that allows to position the load mass
- 4. What if the control input is the voltage E(t)?

Exercise #2

An inertial actuator is a device in which, by appropriate acceleration of an internal mass, a prescribed reaction force can be generated. By attaching the actuator to a structure, the structure motion can be controlled.



The device shown is voice coil driven, where only the winding resistance is important on the electrical side. The mass m is attached to the base with spring k and damper b.

- 1. Here, F_R is the output force. Assume the base has prescribed motion, $v_2(t)$. Construct a bond graph model and derive state equations in port-Hamiltonian form.
- 2. Derive the transfer functions relating F_R to v_2 and F_R to e_c , and denote them with $G_{Fv}(s)$ and $G_{Fc}(s)$, respectively.
- 3. Sometimes we desire the reaction force to mimic the effect of a damper attached between the base and inertial ground, i.e. that $F_R = b_c v_2$, with b_c some controller gain. Derive the ideal control system that will yield the desired reaction force from the inherent dynamics of the device.
- 4. Shown here is the previous device attached to a structure consisting of a mass, m_s , spring, k_s , and damper, b_s . A force, F_d , acts upon the structure mass. Construct a bond graph model for this total system and derive state equations.



5. Derive the open-loop (i.e. with $e_c = 0$) transfer function relating output, v_2 , to input, F_d . Does the result have a component similar to a damper to ground?

Exercise #3

An ideal, compressible, isentropic fluid with one dimensional domain is modelled by the following coupled PDEs that express the conservation of mass and momentum:

$$\frac{\partial \rho}{\partial t}(t,z) = -\frac{\partial(\rho v)}{\partial z}(t,z) \qquad \qquad \frac{\partial(\rho v)}{\partial t}(t,z) = -\frac{\partial}{\partial z}[\rho(t,z)v^2(t,z) + P(t,z)]$$

in which $\rho(t, z) > 0$ is the fluid density, v(t, z) is the flow velocity, P(t, z) is the flow pressure, and $z \in [a, b]$ the spatial coordinate.

1. Prove that the second relation can be equivalently rewritten as

$$\frac{\partial v}{\partial t}(t,z) = -v(t,z)\frac{\partial v}{\partial z}(t,z) - \frac{1}{\rho(t,z)}\frac{\partial P}{\partial z}(t,z)$$

2. The energy variables are in fact the fluid density ρ and its velocity v, and the total energy is

$$H(\rho, v) = \int_{a}^{b} \left[\frac{1}{2} \rho v^{2} + \rho U(\rho) \right] dz$$

where $U(\rho)$ is the internal energy of the fluid. Since $RT \rightarrow \partial U$

$$P(t,z) = \frac{M}{M}\rho(t,z) = \rho^2(t,z)\frac{\partial \theta}{\partial \rho}(\rho(t,z))$$

where R is the universal gas constant, T is the system (constant) temperature and M is the fluid molar mass, compute the expression of the internal energy $U(\rho)$, and write the system of coupled PDEs in port-Hamiltonian form.

3. The co-energy variables are the dynamic pressure and fluid flow, that are given by $\delta H_{(n,v)}$ $\delta H_{(2,\nu)}$

$$\frac{\overline{\delta \rho}}{\delta v}(\rho, v) = \frac{\overline{\delta v}}{\delta v}(\rho, v)$$

Compute their expression.

- 4. The boundary inputs are chosen in the following way: in z = a, the fluid flow, while in z = bthe dynamic pressure. Determine the dual outputs such that the system is in impedance form.
- 5. For stabilisation purposes, a control law based on damping injection is implemented at both sides of the spatial domain. Write down the control law.
- 6. Under the condition $|v(t,z)| \le \sqrt{\frac{RT}{M}}$, prove that the original system can be mapped into $\frac{\partial}{\partial t} \begin{pmatrix} \bar{x}_{-} \\ \bar{x}_{+} \end{pmatrix} + \begin{pmatrix} \lambda_{-}(\bar{x}_{-}, \bar{x}_{+}) & 0 \\ 0 & \lambda_{-}(\bar{x}_{-}, \bar{x}_{+}) \end{pmatrix} \frac{\partial}{\partial z} \begin{pmatrix} \bar{x}_{-} \\ \bar{x}_{+} \end{pmatrix} = 0$

where $\bar{x}_{-}, \bar{x}_{+}, \lambda_{-}, \lambda_{+}$ have to be computed. Verify that, under the previous hypothesis, λ_{-} and λ_+ have opposite sign. Write down the damping injection control law in the new coordinates.

Exercise #4

The figure below shows a planar 2DOF manipulator with rotational joints where:

- A. Each link can be modelled as a homogeneous rectangular bar with mass m_i and moment of inertia I_i around the *z*-axis.
- B. Each joint is subject to a rotational viscous friction with damping coefficient b_i .
- C. θ_i represents the joint variables
- D. Each joint can be actuated by a torque τ_i .
- E. The gravity force is along the negative *y* direction.



Now, answer the next questions:

- 1. Build the port-Hamiltonian model of the manipulator in the joint space.
- 2. Using the control by interconnection technique, build a controller for stabilising the configuration $(\theta_1, \theta_2) = (\pi/2, \pi/2)$. Write down the Casimir function you used for developing the controller.
- 3. Suppose that the robot is under-actuated, i.e. that $\tau_1 = 0$. Is it still possible to stabilise the robot at $(\theta_1, \theta_2) = (\pi/2, \pi/2)$? Which configurations can you stabilise using the control by interconnection technique?