Optimization-based motion planning

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 - Safety constraints. Static obstacles

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The cost should then be designed such that the *planned path* minimizes, in some sense, the deviation from the *reference path*.

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The planned motion is periodically updated based on the current vehicle and environment state, and sent to motion control layer.

Architecture



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- Apply the first element in the control sequence to the process, discard the rest of the sequence, and return to step 1.



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 $\hat{y}(k+1|k),\ldots,\hat{y}(k+N|k)$

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Solution Increment time k := k + 1 and go to 1.

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- The receding horizon principle
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$$V_N(x(0), u(0:N-1)) = \sum_{i=0}^{N-1} (x^{\top}(i)Qx(i) + u^{\top}(i)Ru(i)) + x^{\top}(N)P_f x(N)$$
$$= \sum_{i=0}^{N-1} l(x(i), u(i)) + l_f(x(N))$$
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Remark 1: All x(i) are functions of x(0) and u(0:N-1) via the model (1)! Remark 2: The first term $x^{\top}(0)Qx(0)$ in the objective is really redundant but is

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Space-domain. With (3) as prediction model, the problem is formulated over a finite-distance ahead. Cost, reference and constraints needs to be defined w.r.t. the traveled distance *s*.

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Define the tracking errors $e_x = x - x^r$, $e_u = u = u^r$.



Quadratic cost. Squared, 2-norm of the distance from the path

$$V_N(x(0), u(0:N-1)) = e_x(N)^\top P_f e_x(N) + \sum_{i=0}^{N-1} e_x^\top(i) Q e_x(N)(i) + e_u(i)^\top(i) R e_u(i).$$

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Strongly penalizes large deviation from the path.

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The minimization of V_N results into a linear cost.

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 - constant curvature arcs,

$$\begin{array}{cccc} & x(s) & = P_1^x + R_1 \sin \frac{s}{R_1}, \\ & y(s) & = P_1^y - R_1 \left(1 - \cos \frac{s}{R_1} \right), & 0 \le s \le l_1 \\ & l_1 = R_1 \frac{\pi}{2}, & r_1 = \frac{1}{R_1}, & \psi(s) & = -\frac{s}{R_1}, \\ & l_2 = R_2 \frac{\pi}{2}, & y(s) & = P_2^x + R_2 \left(1 - \cos \frac{s-l_1}{R_2} \right), \\ & & y(s) & = P_2^y + R_2 \sin \frac{s-l_1}{R_2}, & l_1 \le s \le l_2 \\ & & \psi(s) & = -\frac{\pi}{2} + \frac{s-l_1}{R_1}, \end{array}$$

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$$x(s) = \int_0^s \sin \tau^2 d\tau, \quad y(s) = \int_0^s \cos \tau^2 d\tau, \quad \psi(s) = s^2.$$

The curvature is $\rho = 2s$ and the resulting curve is



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The additional control input v is used to avoid aggressive maneuvers due to obstacles that may lead to large tracking errors.

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In case a bicycle model is used to plan the motion, motion planning and control can be lumped together into a single task.

Let's rewrite the kinematic model in the space domain, w.r.t. a reference path ($x^{\sigma}(s), y^{\sigma}\sigma(s)$).



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Define the deviation and orientation error w.r.t. the path in terms of the vehicle pose in the global frame

$$\begin{split} e_y &= \cos\psi^\sigma (Y-y^\sigma) - \sin\psi^r (X-x^\sigma), \\ e_\psi &= \psi - \psi^\sigma. \end{split}$$



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The component v^{σ} of the vehicle speed parallel to the path

$$v^{\sigma} = (\rho^{\sigma} - e_y)\dot{\psi}^r,$$

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$$\begin{aligned} \frac{de_y}{ds} &= e'_y = \frac{1}{V_s} \left(V_x \sin e_\psi + V_x \frac{l_r}{l_f + l_r} \delta \cos e_\psi \right), \\ e'_\psi &= \frac{V_x \delta}{V_s (l_f + l_r)} - \frac{1}{R(s)}, \\ V'_x &= \frac{\dot{V}_x}{V_s}, \end{aligned}$$

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Note that, all variables are to be expressed in the space domain (they are function of *s*).

Safety constraints. Static obstacles

By rewriting the vehicle model in the space domain, where the coordinates describe the vehicle position and orientation w.r.t. the reference path, the safety constraints simply become

$$e_y(s) \in \left[-\frac{L_w(s)}{2}, \frac{L_w(s)}{s}\right],$$

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Assuming the position within the lane of *static obstacles* is provided by a sensing system,

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collision avoidance constraints are imposed by

$$e_y(s) \in \left[-\frac{3L_w(s)}{2}, \frac{L_w(s)}{s}\right] \setminus \mathcal{X}^{obs}, s \in [s^{obs,min}, s^{obs,max}]$$